


10/587929  
IAP11 Rec'd PCT/PTO 01 AUG 2006

Verification of Translation

I, Gabriele Fuchs, residing at Martin-Albert-Str. 4, 90491 Nuremberg, Federal Republic of Germany, hereby declare that I am conversant with the English and German languages and that I am a competent translator thereof. I declare further that, to the best of my knowledge and belief, the forgoing is a true, faithful, complete and accurate translation of PCT/DE2005/000070, filed on January 20, 2005, in the name of Conti Temic microelectronic GmbH the original of which has been submitted to me in the German language.

Nuremberg, May 30, 2006

  
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AUGUST 1 2006

METHOD FOR DETECTING THE BEGINNING OF COMBUSTION IN AN  
INTERNAL COMBUSTION ENGINE

5 The invention relates to a method for detecting the beginning of combustion in an internal combustion engine comprising several cylinders by means of a rotation speed signal determined for a shaft of the internal combustion engine.

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With an in particular self-igniting internal combustion engine it may happen that the combustion in the respective cylinders does not take place at the best possible point of time. This undesired deviation is due to aging effects or  
15 manufacturing tolerances. This may result in an increase of exhaust gas discharge, a rise of fuel consumption or also a deterioration of the concentric running of the internal combustion engine.

20 Methods are known, which detect the exact point of time of the beginning of combustion by means of additionally provided sensors. In DE 33 02 219 A1 as well as in DE 197 49 817 A1 methods are described, which determine the march of pressure in the cylinder internal space by means of  
25 pressure sensors. Furthermore, with DE 25 13 289 A1, DE 44 13 473 A1 and DE 196 12 180 C1 methods are disclosed, which detect the impact sound at the outside of the housing of the internal combustion engine. Based on the pressure and/or impact sound signals measured in this way conclusion  
30 can be drawn to the beginning of combustion of the internal combustion engine. The sensors additionally necessary with known methods stand for considerable additional expenses.

It is the object of the invention to indicate a method of  
35 the above-described type, which permits detection of the beginning of combustion with means which are as easy as

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possible.

This object is achieved by the features of claim 1. As a rule, the method according to the invention can do without  
5 any additional sensor technology. As a measurand it is based merely on the rotation speed signal, which, as a rule, is detected anyway and thus is already available in a control device of the internal combustion engine. Beyond this, the exact beginning of combustion can be easily  
10 detected on the basis of the cylinder signal transformed into the angle frequency range. For this purpose no extensive arithmetic operations occur. For transformation into the angle frequency range it can be reverted, if necessary, to signal transformation methods anyway existing  
15 in the control device.

Special embodiments of the method according to the invention become apparent from the dependent claims.

20 The objects of claims 2 and 3 each concern an advantageous method for generating the cylinder signal, which contains the information to be evaluated of the right now relevant cylinder.

25 The embodiments according to claims 5 to 9 concern favorable possibilities for signal improvement, which are performed in particular before transformation into the angle frequency range. By means of these upstream method steps the beginning of combustion can be determined even  
30 more exactly, since in this case also the signal information, which can be taken in the angle frequency range and which is relevant in this regard, can be determined with higher accuracy.

35 In accordance with the embodiment according to claim 10 the operational behavior of the internal combustion engine can

be improved by using the detected exact beginning of combustion for (post-)regulating the concerned cylinder. The inadequacies initially described can then be largely avoided.

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Preferred examples of embodiment as well as further advantages and details of the invention will now be described taken in conjunction with the drawings. For clarification the drawing is not drawn to scale and certain 10 aspects are shown only schematically, in which

Fig. 1 shows a first example of embodiment of the method for detecting the beginning of combustion and

15 Fig. 2 shows a second example of embodiment.

In Figs. 1 and 2 like elements refer to identical reference numerals.

20 The first example of embodiment shown in Fig. 1 serves for detecting the beginning of combustion of an in particular self-igniting internal combustion engine 1, which comprises four cylinders 2, 3, 4 and 5. However, the number of cylinders is only exemplary. The method can also be applied 25 to an internal combustion engine 1 with a different number of cylinders. A transmitter wheel 7 is mounted to a shaft 6, in particular the crank shaft, of the internal combustion engine 1, which comprises equidistant markings distributed along its circumference. These markings not 30 shown in detail in the example of embodiment can be formed for example in the shape of teeth or even holes. A sensor 8 associated with the transmitter wheel 7, for example in the form of an inductive transmitter, supplies a signal exactly at that moment, at which one of the markings moves along 35 the sensor 8. This signal is supplied to a control device 9.

Apart from other units not shown the control device 9 comprises also sub-units determined for detecting the beginning of combustion. These are a rotation speed unit 10, an averaging unit 11, a transmitter wheel correction unit 12, a signal reconstruction unit 13, a segmentation unit 14, an analysis unit 15 and a controller 16. These sub-units can be available physically separated, e.g. as separate electronic sub-assemblies or also combined to a single physical unit. The latter is possible on a signal processor particularly in case of a program technical implementation of the sub-units 10 to 16. A mixed form is also possible.

In the following the functioning of the detection of the beginning of combustion and its post regulation are described more detailed. The time domain signal delivered by the sensor 8 is converted in the rotation speed unit 10 into a rotation speed signal, which - as is usual with the control of internal combustion engines - refers to the rotation angle range. Depending on the rotation angle of the shaft 6 the rotation speed signal indicates the respective current shaft rotation speed or the shaft rotation acceleration.

25

Subsequently, a segment signal SS with a rotation angle range is extracted from the rotation speed signal, within which each of the cylinder 2 to 5 ignites exactly one time. In case of the example of embodiment this is a segment that corresponds to a duplicate full rotation of the shaft 6, i.e. with a 720 degree rotation angle range. However, depending on the type of the internal combustion engine 1 or on the shaft 6 used for detecting the rotation speed signal, which instead of the crank shaft could be formed also as a camshaft, the rotation speed range of the segment signal SS basically can be differently sized.

At present, detection of the rotation speed signal and also of the segment signal takes place practically in each control device 9 of an internal combustion engine 1.  
5 Consequently, these are no detecting means provided separately for the detection of the beginning of combustion.

The method steps described in the following always start  
10 from the existence of a quasi stationary operational state of the internal combustion engine 1.

The method steps, which are taken in the averaging unit 11, in the transmitter wheel correction unit 12 and in the  
15 signal reconstruction unit 13 are optional. They serve for improving the signal quality of the segment signal SS. In the end, the higher its quality, the more exactly the beginning of combustion can be determined.

20 In the averaging unit 11 the arithmetic mean value of two or more successive segment signals SS is formed. By means of this in particular cyclical variations, which come for instance from an unsteady combustion, can be eliminated.

25 Due to mechanical manufacturing tolerances inaccuracies may occur at the markings arranged at the transmitter wheel 7. Thus, these markings cannot be located at equidistant distances from each other. The inaccuracies caused hereby in the segment signal SS can be eliminated on the basis of  
30 known correction methods. In DE 41 33 679 A1, DE 42 21 891 C2 and DE 196 22 042 C2 such correction methods are described. Here, correction values are detected, which are deposited in the control device 9, and by means of which the rotation speed signal and also the segment signal can  
35 be released from the mentioned transmitter wheel errors.

A further possibility for signal improvement is to use a signal reconstruction method. The markings on the transmitter wheel 7 are usually located at rotation angle distances of 6 degrees or even 10 degrees. Here, however, 5 the rotation speed of the shaft 6 is scanned too inaccurately for some applications. Present established applications, such as for example smoothness control or also combustion beginning control work more efficiently if a higher scanning rate is available. Use of the transmitter 10 wheel 7 with a larger number of markings, however, is not unproblematic, as with an increasing number of markings the clear space between the individual markings and thus the risk of contamination enhances. A possible consequence would be the ignoring of individual markings.

15

Nevertheless, however, the scanning rate can be increased by means of certain methods of digital signal processing. A first possibility is an interpolation in the rotation angle range between the scanning values determined by the 20 scanning rate of the transmitter wheel 7. Apart from a simple linear interpolation in particular also a Lagrange-interpolation or a sinc-interpolation is suitable. The Lagrange-interpolation, which is especially advantageous in this respect, is a special polynomial interpolation method. 25 Compared to other interpolation polynomials of a higher rank, which basically can also be used, the Lagrange-interpolation is advantageous in that it can do without the solution of a relatively complex system of equations. The sinc-interpolation is based on a mathematic convolution 30 operation.

In the example of embodiment, with a periodical and band-limited signal the Lagrange-interpolation as well as the sinc-interpolation deliver an exact signal reconstruction 35 to the segment signal SS, while taking into consideration the scanning theorem, whereby they differ advantageously

from a linear and also from another higher-graded polynomial interpolation.

A second possibility for increasing the scanning rate is a  
5 frequency transformation of the segment signal into the  
angle frequency region. This transformation is performed in  
particular by means of a discrete Fourier-Transformation  
(DFT) or a discrete Hartley-Transformation (DHT). Unlike  
the Fourier-Transformation the Hartley-Transformation  
10 beneficially carries out only mere real operations. This  
results in lower computing expenditure. Both  
transformations each provide for an amplitude value and a  
phase value with discrete angle frequencies, which in the  
region of the internal combustion engines are also called  
15 orders. A continuous reconstruction signal for the segment  
signal SS results on the basis of a superposition of  
harmonic partial vibrations of those orders (=angle  
frequencies), for which in the angle frequency range  
relevant spectral portions, i.e. amplitude and phase  
20 values, have been determined. In this case the individual  
harmonic partial vibrations are weighted with the amplitude  
and phase value respectively associated. In this manner and  
when complying to the scanning theorem an exact  
reconstruction of the segment signal SS is possible, as far  
25 as the basic signal is periodical and band-limited.

The interpolation as well as the frequency transformation  
method deliver a reconstructed signal, which exists in form  
of an analytic functional printout. From this the required  
30 functional value can be taken at any places in the rotation  
angle region, i.e. in particular also between the  
metrologically determined scanning places. This results in  
the desired higher scanning rate. Thus, from a segment  
signal SS with an original scanning rate of 10 degrees a  
35 modified segment signal with an arbitrary higher scanning  
rate, e.g. with a 0.1 degree-scanning, can be generated.



The particularly advantageous Lagrange-interpolation method as well as the mentioned Frequency-Transformation method (DFT, DHT) can be realized as so-called FIR-filter (=finite  
5 impulse response). Basically, however, also other forms of implementation are possible.

After having passed through the sub-units 11, 12 and/or 13 provided for signal improvement an improved segment signal  
10 SS\* is available, which indicates the information on the beginning of combustion in the cylinders 2 to 5.

In the segmentation unit 14 the improved segment signal SS\* is decomposed into a total of four cylinder signals ZS1,  
15 ZS2, ZS3 and ZS4. Each cylinder signal ZS1 to ZS4 then merely indicates the information on ignition in a single cylinder. In doing so, in the present example of embodiment the cylinder signals ZS1 to ZS4 can detect an angle range of up to 180 degrees. However, from the improved segment  
20 signal SS\* an extraction of cylinder signals ZS1 to ZS4 is favorable, which comprise only an angle range, within which the actual ignition process effectively takes place in the respective cylinder 2 to 5, i.e. in particular the range lying respectively around the top cylinder dead center. For  
25 this purpose, for example a rotation angle range of approx. 40 to 50 degrees is sufficient.

The cylinder signals ZS1 to ZS4 determined in this way are supplied to the analysis unit 15, which performs for each  
30 cylinder signal ZS1 to ZS4 a frequency transformation into the angle frequency range. This, in turn, can happen by means of a DFT, a DHT or a digital filtering, for example in form of a digital bandpass-filtering with variable mid-frequencies or in form of digital filter banks. This  
35 transmission into the angle frequency range produces from the cylinder signals ZS1, ZS2, ZS3 and ZS4 respectively

associated cylinder frequency signals FS1, FS2, FS3, respectively FS4. In this case, for the latter, in turn, amplitude values and phase values with associated discrete angle frequencies are available.

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This signal information, i.e. the angle frequencies plus their associated amplitude and phase values, indicate the information included in the basic respective cylinder signal ZS1 to ZS4 on the operational state in the  
10 respective cylinder 2 to 5. In particular, from this signal information also the exact beginning of combustion in the respective cylinder 2 to 5 can be taken in easy manner. This can take place by means of a comparison with for example empirical experience values or also with reference  
15 values determined in advance. The experience and/or reference values are preferably deposited in the analysis unit 15. It can also be reverted to the signal information of the particularly signal-strong angle frequencies. For this purpose preferably those angle frequencies come into  
20 question, for which the amplitude value lies above a threshold, in particular above the 3dB-threshold. The signal information, preferably the phase information, of the special angle frequency thus determined is then made available as the combustion beginning signal BS1, BS2, BS3  
25 and BS4 of the analysis unit 15 reproducing the beginning of combustion in the respective cylinder 2 to 5.

The combustion signals BS1 to BS4 are supplied to a controller 16, which uses the included information on the  
30 beginning of combustion for (post-)regulation of the respective cylinder 2 to 5, at least as far as this is still categorized as admissible by a higher-ranking controller limitation possibly available. The (post-) regulation can take place for example by means of a  
35 variation of the starting output at a fuel-injection pump of the internal combustion engine 1 not shown in detail. In

particular the regulation can be performed on the basis of at least one load and/or rotation speed dependent phase-starting output-curve family. Hereby, individually for each of the cylinders 2 to 5 the beginning of combustion is  
5 adjusted to the optimum point of time. This is possible in particular without substantial additional hardware components becoming necessary in the control device 9 or at the internal combustion engine 1 for the above-described method. Particularly no additional detection of special  
10 operating parameters of the internal combustion engine 1 is necessary. This results in a very cost-efficient realization for the detection of the beginning of combustion and for the cylinder-individual post regulation of the point of time of the beginning of combustion.

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With reference to Fig. 2 a second example of embodiment of the invention is described in the following. Identical elements refer to like reference numerals as is the case with the first example of embodiment, to which description  
20 reference is made herewith. The essential difference is the replacement of the segmentation unit 14 by an adjustment unit 17, which in the second example of embodiment is directly connected after the rotation speed unit 10.

25 The adjustment unit 17 functions substantially to adjust for example the cylinder 2, for which the beginning of combustion is to be currently detected, such that the signal portion caused by the cylinder 2 in the resulting rotation speed signal or segment signal SS, respectively,  
30 dominates clearly in relation to those of the other three cylinders 3 to 5. In this case the segment signal SS is practically exclusively determined by the currently relevant cylinder 2. Adjustment of the operational state takes place for example by a targeted increase of the  
35 supplied fuel quantity. However, in principle, other adjustment possibilities are also feasible.

Based on the dominance of the signal portion, caused by the adjusted cylinder 2, in the segment signal SS there is no necessity of a further segmentation in the segmentation unit 14 according to the first example of embodiment. The improved segment signal SS\* is used as a whole as cylinder signal ZS1. The other method steps proceed analogue to the first example of embodiment, however provided that only for the relevant cylinder 2 a combustion beginning signal BS1 is generated by the analysis unit 15. As a consequence, in this method cycle only the cylinder 2 can be post regulated. For the remaining cylinders 3 to 5 this happens thereafter in sequential chronology. The adjustment unit 17 successively adjusts significantly the operational state in one of the remaining cylinders 3 to 5, respectively. Advantageously, the adjustment unit 17 intervenes only if the internal combustion engine 1 has reached its quasi stationary operational state. This can be easily established by means of the rotation speed signal determined in the rotation speed unit 10 or also by the segment signal SS.